



A FEM APPROACH TO STUDY AND ANALYSE OF VIBRATION IN PROSTHETIC KNEES IMPLANTATION

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Abstract : FEM has been extensively utilized in engineering and quantitative modeling to numerically resolve differential equations. This research has examined the impact of swinging phases, mandibular and other variables and overweight of total knee substitutions using a finite element technique. Finite element has been utilized to investigate and assess complete joint replacements for mechanical behavior. Total joint substitutions are increasingly being used in the concept, research, and pre-clinical examinations.

IndexTerms - knee replacements, prosthetic knees implant, FEM approach.

I. INTRODUCTION

The prosthetic knee joint has been a topic of great interest in the past. Over time, various researchers have worked on the prosthetic knee joint trying to address the issues like geometric modeling, stress analysis between the articular surfaces, reliability, and fatigue life, wear, dynamic analysis, etc. A large amount of literature is available in this regard. Artificial knee joints can be divided into mechanical and computer types. Mechanical knees can be divided into uniaxial knees and multiaxial / multicentral knees. All knee replacements require some form of a stabilization mechanism. This is a manual or weight- actuated locking system. We also need a way to control flexion and extension movements. Knee replacement is the surgical replacement of the knee joint, where the femur and tibia meet, with an artificial joint or implant. This process may seem modern but dates back to the mid-19th century. Medical technology companies have advanced all types of artificial joints over the last three decades as doctors have discovered a growing demand for artificial joints. Younger (and more active) potential recipients are tired and injured in their joints, demanding permanent or semi-permanent medical solutions. Doctors recommend knee **replacement if the patient is suffering from constant pain or if daily activities are affected by limited mobility**. According to the American Academy of Orthopaedic Surgeons, more than 90% of knee replacement patients experience a significant reduction in knee pain. Recipients may undergo partial or complete knee arthroplasty. The difference depends on the recipient's condition and the level of pain. To verify the artificial knee's functionality following a transplant, a comprehensive investigation of load, dynamic behavior, and wear prediction is necessary. There was no avoiding the fact that finite element analysis will serve as a computational approach for biomedical as well as other technical hurdles. Researchers have looked into both non-contact and contact analysis to better comprehend the prosthetic knee joint's behavior. It was necessary to investigate the impact of bone deformations on contact behavior, so the convergence of finite element solutions was analyzed. Precise solutions for femorotibial contact behavior are obtained by treating the bones as rigid. The articular surfaces of the femoral condyles were measured along their sagittal axis with a laser rangefinder, and the average of these measurements was then used to conduct a femorotibial contact analysis. The stress predictions are sensitive to the mesh resolution. Reproducing the kinematics, contact pressure distribution, and contact area of a deformable system is the goal of the rigid body analysis.

II. METHODS AND MATERIAL

2.1 Dynamic Analysis: The three-dimensional dynamic response of the human knee joint has been studied and reported that most isolated posterior cruciate ligament injuries and combined posterior cruciate and medial collateral ligament injuries are due to posterior impact on the flexed knee. The dynamic multibody musculoskeletal model can predict muscle strength and joint contact pressure at the same time.

2.2 Thermal Analysis: Polymers, which are used as biomaterials for tibial components, change their properties significantly as a function of temperature. Friction creates surface heat during the range of motion throughout the knee, leading to damage and breakage of the ultra- high molecular weight polyethylene tibial insert. The performance of the prosthesis should minimize the effect of heat on the surface of the joint component.

Following are the objectives of work

- 1) Acceleration and maximal pressure differences are evaluated between set and telephone knee implants during each step in

the gait cycle.

- 2) Determining the cost-effectiveness of lifelong knee pain.
- 3) Indication of efficiency in a range of situations with static and wireless arrangement inserts.
- 4) To measure the deepness and effect of the tibial part on the pressure of the tibial bearing.

Details of material used are as the materials used are Cobalt Chromium Alloy, Nitinol, Ti-6Al-4V

2.3 Numerical Modelling: Composite beams gleaned from experiments and numerical applications, in particular the "A3" model, are put to use in this endeavour. The finite element model was created with the same geometries, parameters, material properties, and lingo as the composite beams.

2.4 Material Modelling: The finite elements in the ANSYS code standard library were used to define the proposed numerical model. SOLID186, a 20-node high-order 3D solid element was used. Non-linear spring elements (ANSYS COMBIN39) and (Beam 189) are used to represent the behaviour of chemical anchors. COMBIN39 is used to resist the normal force between the concrete and the steel beam. COMBIN39 is a non-linear generalized force-deflection unidirectional element (or non-linear spring) that is used in the analysis. Concrete compressive strains of 0.2% and 0.35% are used to define the lower and upper bounds, respectively.

2.5 Geometry: Geometry used is shown in Figure.1

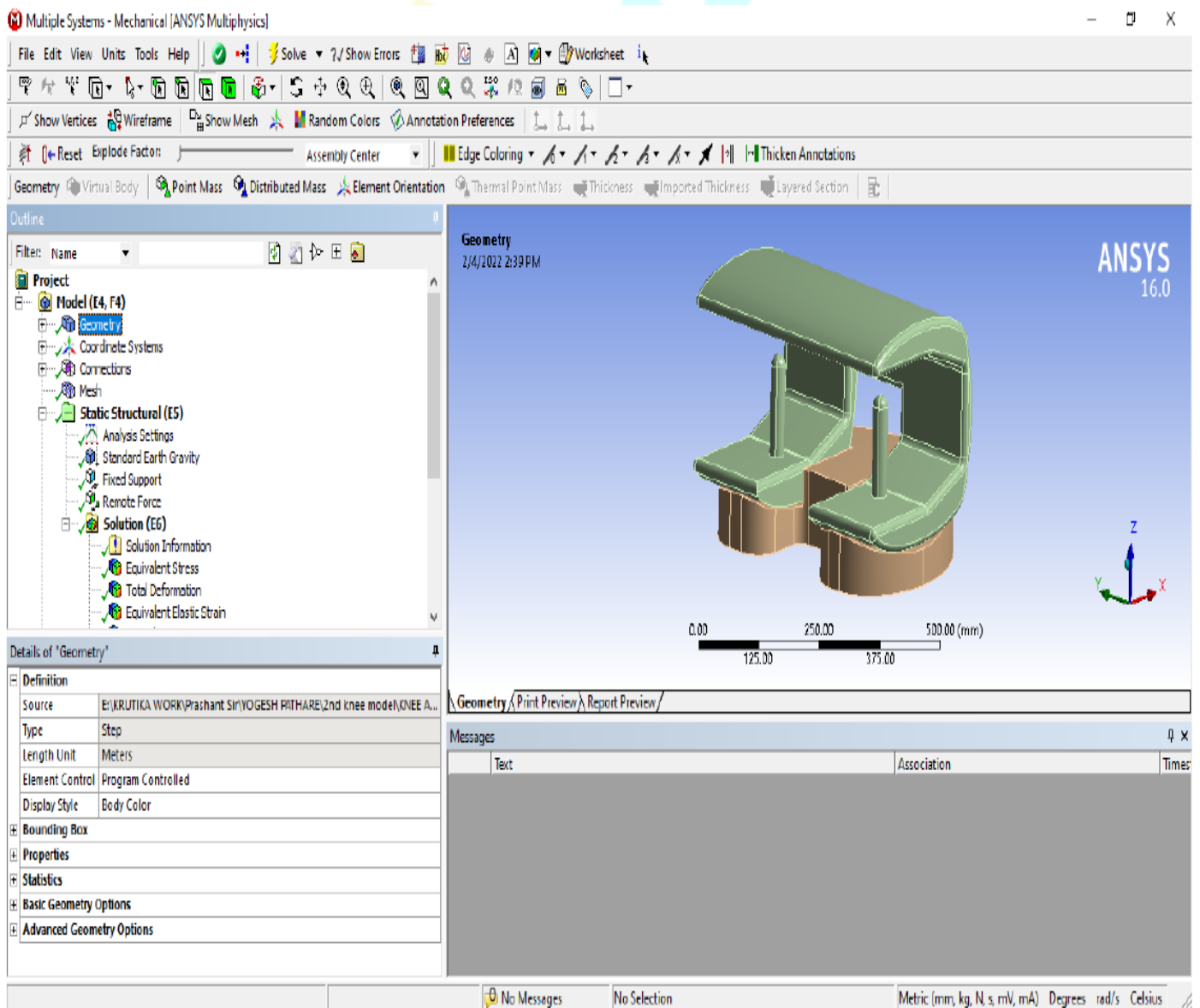


Fig. 1:Geometry

2.6 Meshing: Meshing carried out is shown Figure.2

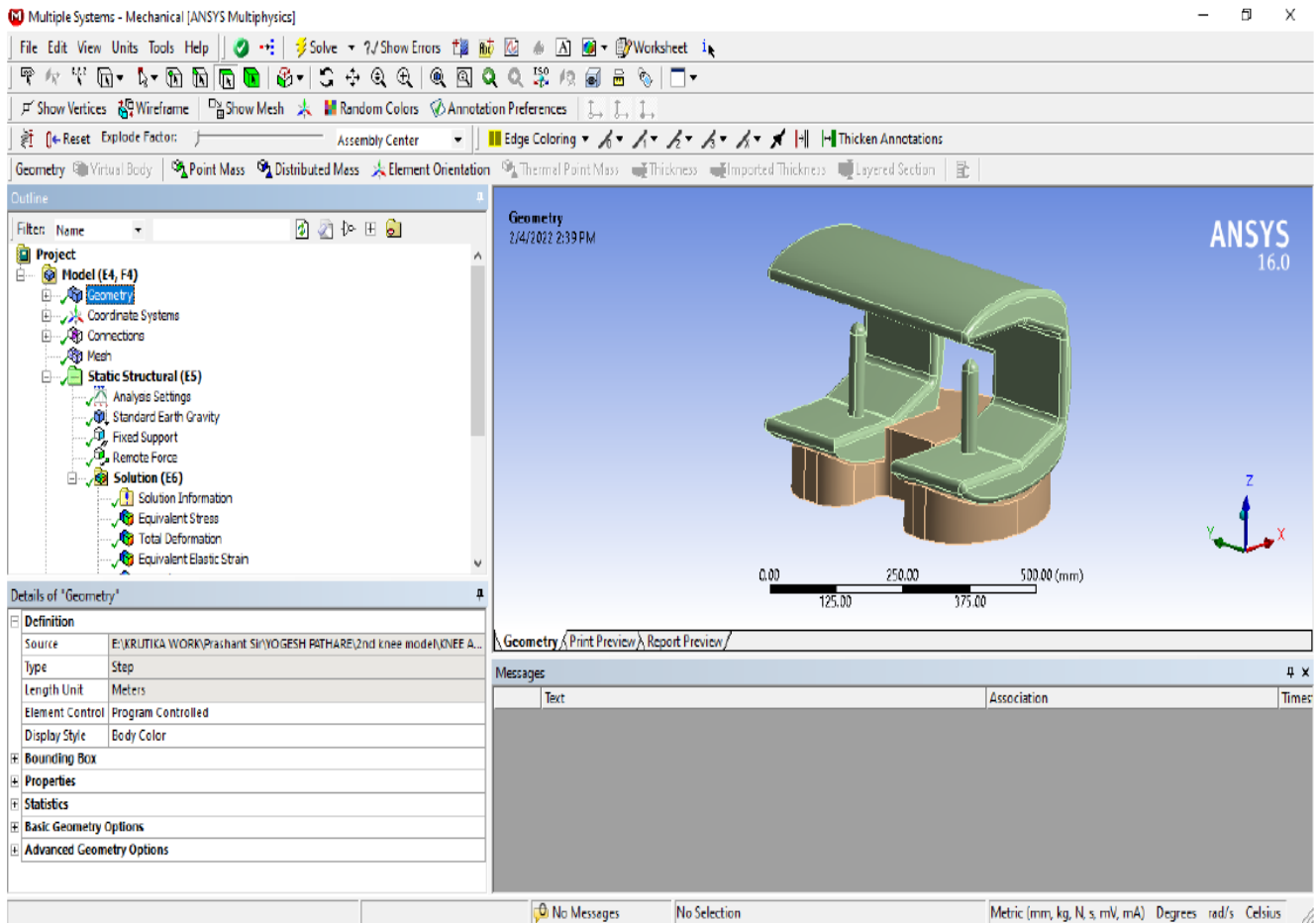


Fig. 2: Meshing

2.7 Total Deformation: Total deformation obtained for CoCr is shown in Figure.3

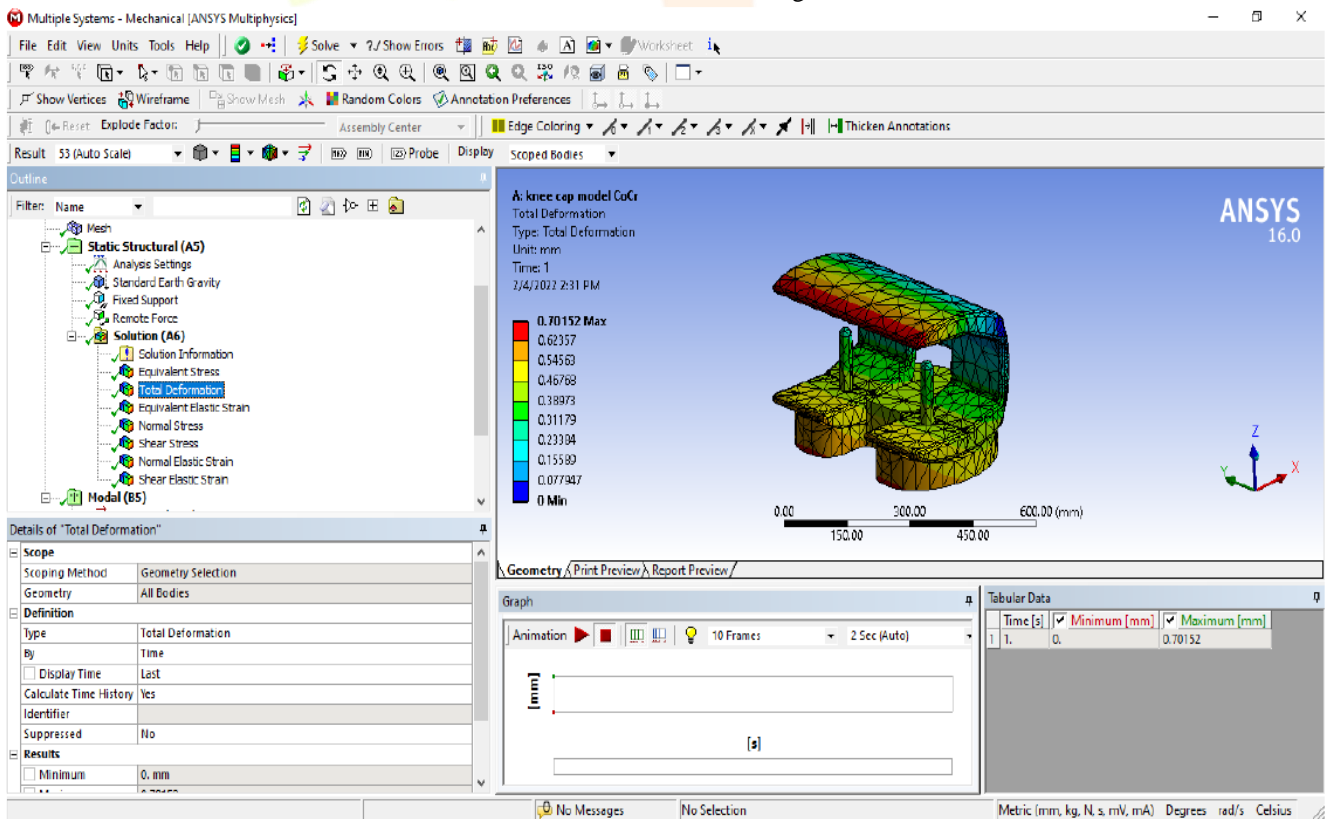


Fig. 3. CoCr Total Deformation

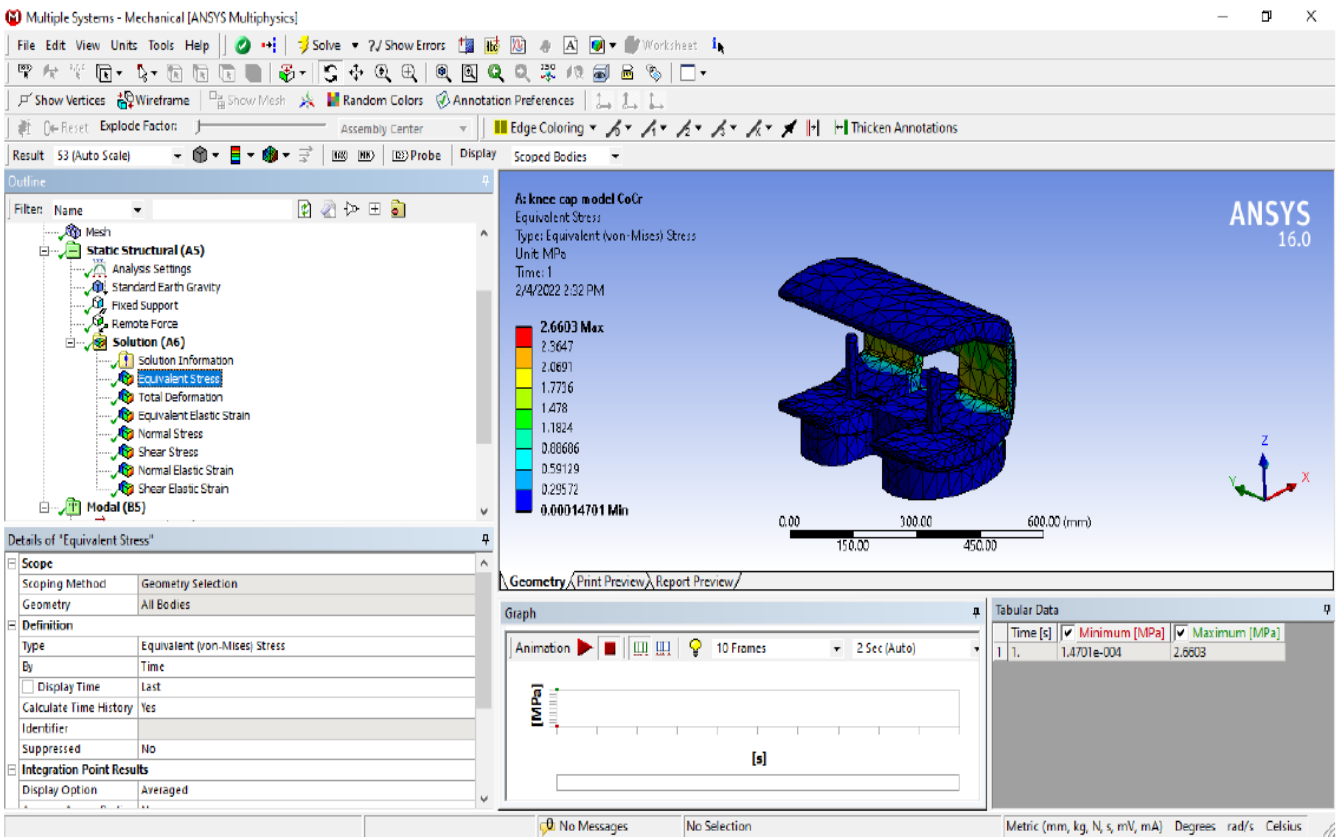


Fig. 4. CoCr Equivalent Stress

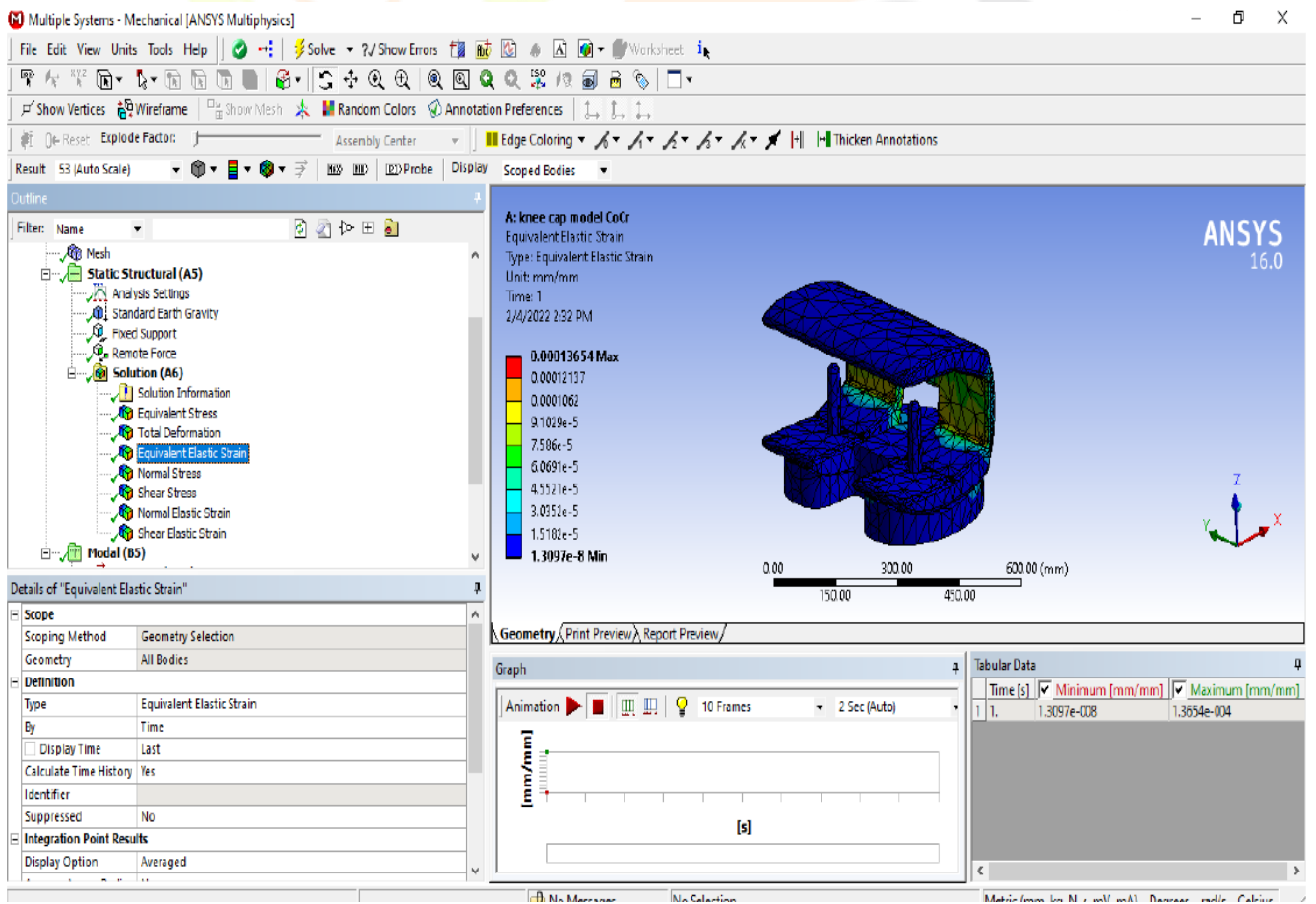


Fig. 5. CoCr Equivalent Elastic Strain

Figure 4, 5 and 6 are showing Equivalent Stress, Equivalent Elastic Strain, and Normal Stress for CoCr respectively.

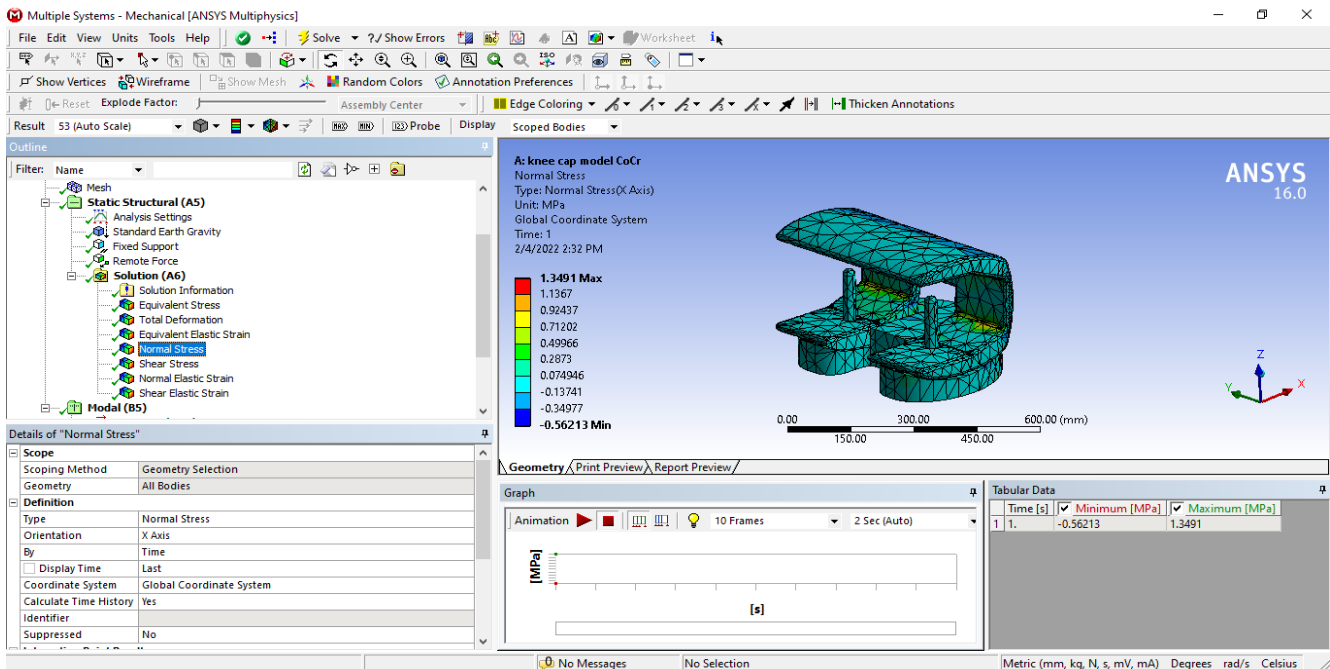


Fig. 6. CoCr Normal Stress

III. RESULTS , DISCUSSION

Total Deformation: Total deformation obtained is shown in Table1.Total deformation Comparison is shown in Figure 7

Table1: Total Deformation (mm)		
Kneecap model materials		
Co-Cr	Ti6Al4V	Ni-Ti
0	0	0
0.077947	0.070244	0.056976
0.15589	0.140490	0.11395
0.233833	0.210736	0.170924
0.311776	0.280982	0.227898
0.389719	0.351228	0.284872
0.467662	0.421474	0.341846
0.545605	0.49172	0.39882
0.623548	0.561966	0.455794
0.701491	0.632212	0.512768

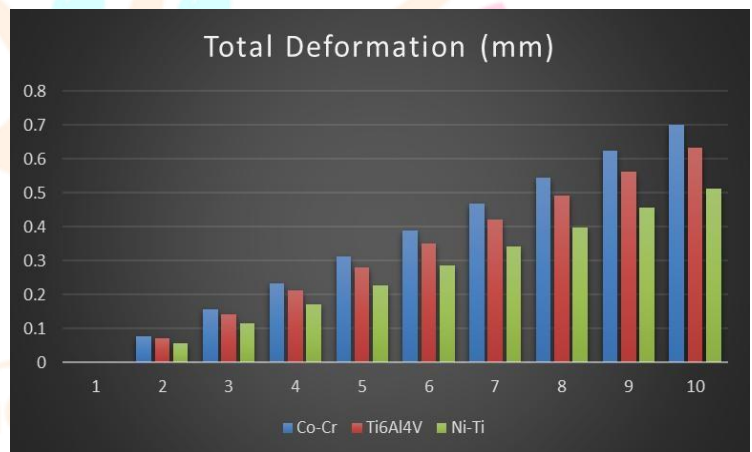


Fig. 7. Total Deformation Comparison Bar Diagram

Equivalent Stress: Equivalent Stress obtained is shown in Table 2.Equivalent Stress comparison is shown in Figure 8

Table 2: Equivalent Stress (mm)		
Kneecap model materials		
Co-Cr	Ti6Al4V	Ni-Ti
0	0	0
1.09E-05	1.00E-05	0.000147
1.4477	1.23	0.29572
2.90E+00	2.65E+00	0.591293
4.343078	4.19	0.886866
5.79E+00	5.65	1.182439
7.238457	7.13E+00	1.478012
8.69E+00	8.61	1.773585
10.13383	10.09	2.069158
1.16E+01	1.13E+01	2.364731

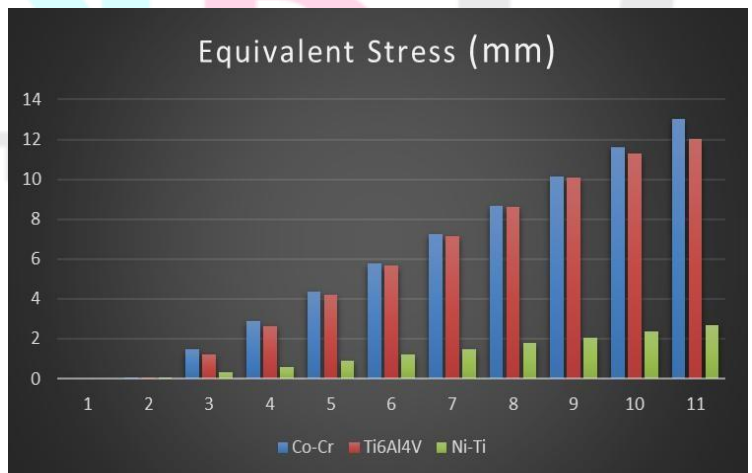


Fig. 8: Equivalent Stress Comparison Bar Diagram

Similarly Normal Stress, Normal Elastic Strain, Shear Stress, Shear Elastic Strain, Equivalent Elastic Strain are obtained.

IV. CONCLUSION

The conclusions can be drawn are as joint can simply sustain a weight of 65 to 70 kg when the weight varies in stable conditions. It can be said during the walking processes i.e., from three coplanar forces that joint wear rises when the stresses are compared to the constant state. The stresses are highly varying in dynamic conditions for the patellar tendon and response force because of running or joint operation in comparison to walking conditions which produce joint injury.

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