

## "Low Energy Cooling Technique For Office Space In Mumbai"

<sup>1</sup>Krish Bhagat, <sup>2</sup>Rohan Chavan, <sup>3</sup>Om Ghag, <sup>4</sup>Sahil Ghosalkar, <sup>5</sup>Prajakta Kane

<sup>1</sup>Mechanical Engineering <sup>1</sup>SIES G<mark>ST</mark>,Nerul,Mumbai

*Abstract*: The demand for effective cooling solutions in office buildings, particularly in regions like Mumbai with high temperatures and humidity levels, presents major challenges for centralised air conditioning systems. Although central air conditioning machines are commonly used, they have some drawbacks, such as high energy consumption and operational costs. To tackle these challenges, this paper presents an alternative technique employing existing HVAC technologies adapted. Variable Refrigerant Flow (VRF) systems, for example, increase energy efficiency by adjusting refrigerant flow rates in response to changing load demands. Energy recovery ventilation (ERV) systems can also be used to save energy by capturing heat and moisture from outgoing air streams. Using this new HVAC technology has several advantages over previous systems. They reduced power consumption significantly for the initial time, which reduced operational costs and their impact on the environment. Furthermore, they boost ventilation and cooling rates, giving workers a more comfortable working environment. Labour costs are reduced by these technologies since they require less workers to run. The abstract also emphasises the supplementary usage of passive cooling techniques to central air conditioning systems, such as roll-up curtains, reflective film, vegetation, thermal insulating walls, and building orientation optimisation. Without relying on mechanical cooling, passive cooling systems employ natural circulation and shade to lower heat buildup and enhance indoor comfort

#### IndexTerms - Component,formatting,style,styling,insert.

I. INTRODUCTION

#### **INTRODUCTION**

Low-energy cooling methods for warm, humid environments In humid and hot cities like Mumbai, the ability to cool spaces effectively and continuously is essential. As the world's population grows and cities get more and more crowded, there is an increasing need for suitable workstations that don't use a lot of energy or hurt the environment. Hot and muggy places can be challenging due to traditional air conditioning systems' discomfort, health hazards, and high energy use. The overall objective of the project is to investigate potential low-energy cooling alternatives in order to address these issues. These suggestions could save costs, preserve the environment, and significantly reduce energy use. Thus, the project's goal is to update the old systems with economically cost, energy-efficient, and environmentally friendly cooling technologies. Mumbai is a humid and swampy city, so offices must have low-energy cooling equipment. They are good at keeping people comfortable while also having a low environmental impact. You can make a difference by using passive cooling methods that rely on natural indications such 2 as the sun and wind. Consider things like heat-regulating walls, plants, reflective film, and attractive roller curtains. Good windows, reflective roofs, and well-insulated buildings can all help to keep interior temperatures comfortable while using minimal energy.

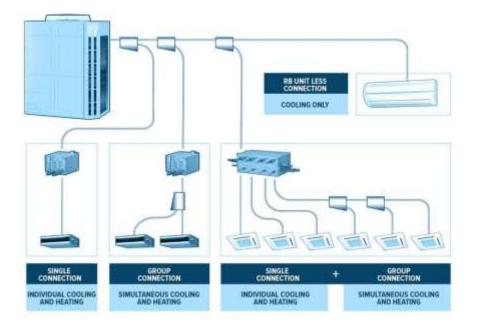
### 1.1 Existing System

In the office space that we have considered the existing system used is the centralised air conditioning system. This system is one of the most commonly used in areas like Office Buildings, Hotels and Hospitality Industry, Shopping Malls and Retail Spaces, Healthcare Facilities, Educational Institutions, etc. Centralized air conditioning (AC) systems are widely used in office spaces for their efficiency, convenience, and cost-effectiveness. Centralized AC systems ensure uniform cooling throughout the office space, eliminating hotspots and ensuring a comfortable working environment for all employees, Centralised air conditioning systems guarantee consistent temperature throughout the organisation, removing discomfort and ensuring that every employee has a comfortable place to work. When it comes to energy efficiency, these systems are meant to be superior to decentralised ones. The need for separate cooling units in each office space is eliminated by centralised air conditioning systems, clearing up valuable floor space that can be used for more workplaces, meeting rooms, or common areas. This maximises the use of office space by reducing overall energy consumption and enhancing energy efficiency. This integration allows for centralised monitoring and control of all building functions while improving overall building efficiency. Office space requirements can be easily adjusted with centralised air conditioning systems. Additional cooling capacity can be added or changed as needed to meet the increasing demand.

In summary, the use of centralised air conditioning systems in office spaces has various advantages, including constant cooling, energy efficiency, space optimisation, centralised control, enhanced indoor air quality, scalability, interaction with building management systems. While meeting the functional requirements in modern office buildings, these systems help to provide a comfortable, effective, and sustainable work environment for employees.

## Proposed System:-

The flow of refrigerant to indoor units is adjusted by variable refrigerant flow (VRF) systems according to demand. The VRF technology is the best choice for applications where zoning is necessary or when changing loads are present because it allows users to manage the quantity of refrigerant supplied to fan coil units spread throughout a building. In situations when simultaneous heating and cooling are necessary, VRF systems can be used as heat pump systems or heat recovery systems. VRF systems not only offer improved comfort but also design flexibility, energy savings, and affordable installation.



### Fig 1.1 VRF System

One outdoor unit may be connected to several indoor fan coil units in a VRF system. The speed of the outdoor unit's one or more inverter-driven compressors can be changed by altering the frequency of the power supply to the compressor. The amount of refrigerant that will be delivered by the compressor changes along with the compressor speed. Each interior fan coil unit has its own metering device, which may be managed by the indoor unit or the outdoor unit. The outdoor unit distributes the amount of refrigerant required to satisfy each indoor unit's specific needs as soon as each indoor unit transmits a demand to it (Fig. 1.2). These features make the VRF system ideally suited for all applications that have part load requirements based on usage or building orientation, as well as applications that require zoning.

## International Research Journal

The VRF systems available on the market today differ according to the number and type of compressor. The 3 types of units that will be compared here are:

- Single Variable Speed Compressor
- Variable Speed Compressor Plus Fixed Speed Compressor
- Multiple Variable Speed Compressors

### Single Variable Speed Compressor:

In this system with a single, large-capacity scroll compressor, the same compressor starts and runs when there is demand and no redundancy is available if the compressor fails.

### Variable Speed Compressor Plus Fixed-Speed Compressor:

In this two-compressor system, the inverter-driven compressor always starts and ramps up until it reaches its maximum capacity at which time the fixed-speed compressor starts, and the inverter driven compressor ramps down. This system provides back-up capability.

### Multiple Variable Speed Compressors:

Outdoor units with multiple inverter-driven twin rotary scroll compressors, offer the most complete set of advantages achievable with a VRF system. Multiple inverter-driven compressors allow the unit to provide better part load performance without the need to use hot gas bypass. Under low-load conditions, the system has the advantage of running only as many compressors at whatever speed is required to achieve the capacity necessary to satisfy the load and maintain comfort within the conditioned space.

### NEED OF THE STUDY.

Having efficient cooling systems in place is crucial to ensuring that office workers can conduct business without discomfort in Mumbai, where heat and humidity are common. This supports the city's environmental goals by increasing output and helping to reduce energy use. This is the exact topic of the unique low-energy cooling experiment currently under way. Using innovative techniques that are especially suited to Mumbai's distinct surroundings, the project aims to leave a lasting impression. The objective is to significantly reduce the amount of energy needed for cooling by the use of a variety of passive cooling techniques, such as reflective film, energy-efficient HVAC systems, creative roller curtains, and thermal insulation. Automation of smart buildings is also used. As a result, this will support preserving each tenant's ideal degree of comfort in these office buildings. In addition, the project will look into the subject of sustainable energy sources, looking for ways to reduce dependency on conventional energy solutions, the initiative aims to lower global carbon emissions and open the door for additional environmental innovations. With the comprehensive low-energy cooling plan, Mumbai has a solid foundation for a more environmentally friendly and sustainable future. The goal of the project is to motivate other communities to work towards a greener, more energy-efficient future.

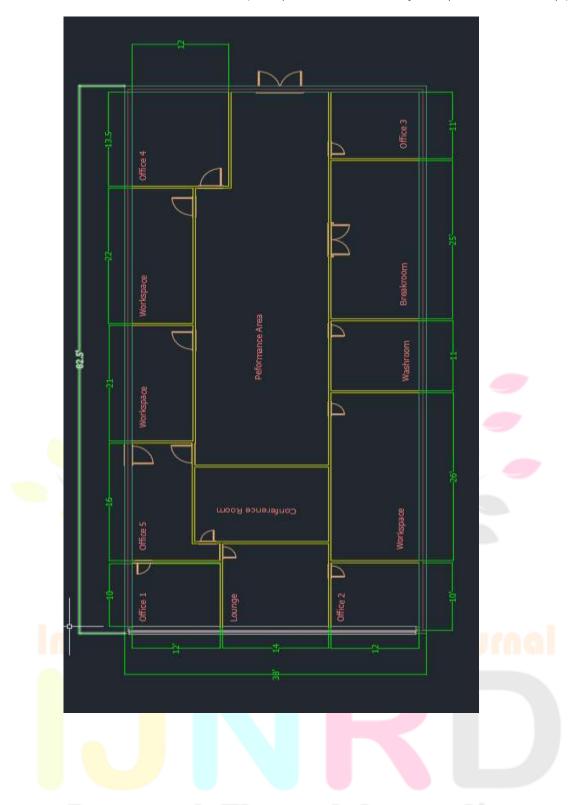
### METHODOLOGY

The design procedure outlines the end-to-end solutions that are required to be taken to determine the appropriate heating, ventilation, and air conditioning (HVAC) system for a Office floor.

The first step involves visiting the location and analysing the site. This may involve assessing factors such as the orientation and position of the building, the climate and weather conditions in the area, and any potential sources of heat or humidity.

Once the architectural layout has been obtained, the next step is to calculate and measure the area that requires cooling. The heat load for each zone is then calculated based on factors such as the size and orientation of windows, the amount of insulation, and the heat generated by occupants and equipment. The cooling load calculation is an important step in the design process, as it provides the information necessary to properly size and select an air conditioning system that will meet the cooling needs of the building or space. The size of the air conditioning system will depend on the calculated cooling load and other factors such as the climate, budget, and energy efficiency requirements.

#### © 2024 IJNRD | Volume 9, Issue 5 May 2024| ISSN: 2456-4184 | IJNRD.ORG



The heat load gives details such as the refrigeration capacity, CFM requirement, and fresh air requirement for each room. Refrigeration capacity refers to the amount of cooling required to maintain a comfortable temperature in the room, while CFM requirement is the volume of air that needs to be circulated to maintain a healthy and comfortable indoor environment. Fresh air requirement refers to the amount of outside air that needs to be brought into the room to maintain good indoor air quality.

Once the refrigeration capacity, CFM requirement, and fresh air requirement for each room have been determined, specific IDUs and ODUs can be selected from manufacturer catalogues. These components must meet technical specifications such as the required cooling capacity, airflow rate, and noise level, as well as cost requirements for the project budget.

IJNRD2405048

In addition to the HVAC system, ventilation systems must also be selected for supply and exhaust ventilation to maintain the required amount of pressure in the room and meet the CFM requirement. Ventilation systems are needed to be designed particularly in places like Toilets.

### Floor Plan:-

### Area calculation sheet

	A	В	C	D	E	F
1		HEIGHT	AREA	VOLUME	OCCUPANCY	EQUIPMENT LOAD
2	ZONE	(Ft)	Sq.ft	Cu.ft	(Nos)	(W)
3	OFFICE 1	11.5	112	1287	2	168
4	OFFICE 2	11.5	112	1287	4	168
5	OFFICE 3	11.5	115	1328	5	173
6	OFFICE 4	11.5	179	2060	4	269
7	OFFICE 5	11.5	149	1715	9	224
8	WORK SPACE	11.5	292	3358	9	438
9	SPACE 1	11.5	139	1600	6	209
10	SPACE 2	11.5	163	1872	9	244
11	BREAK ROOM	11.5	275	3162	9	412
12	CONFERENCE ROOM	11.5	197	2264	10	295
13	LOUNGE AREA	11.5	175	2009	6	262
14	PERFORMANCE AREA	11.5	913	10500	15	1370
15	TOTAL		2821			

### Method 1- Without Any Modification:-

Without Any modification that is without passive cooling technique. Initially to begin with we start the simulation on revit considering the major parameters like singe pane glass, centralised AC system, no insulation and brick wall which did not include and of the passive cooling technique.

# **Research Through Innovation**

Loads Report (7) 🛛 📲 Level 0	Loads Report (9)	Loads Report (10) X
Droject Cummory		
Project Summary		
Location and Weather		
Project		Project Name
Address		
Calculation Time		12 April 2024 13:17
Report Type		Standard
Latitude		19.14°
Longitude		72.88°
Summer Dry Bulb		32 °C
Summer Wet Bulb		25 °C
Winter Dry Bulb		17 °C
Mean Daily Range		5 °C
Building Summary		
Inputs		
		Office
Inputs		Office 2,943
<b>Inputs</b> Building Type		
<b>Inputs</b> Building Type Area (ft <sup>2</sup> )		2,943
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF)		2,943
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results		2,943 33,842.95
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton)		2,943 33,842.95 16.221
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour		2,943 33,842.95 16.221 July 16:00
Inputs Building Type Area (It <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton)		2,943 33,842.95 16.221 July 16:00 12.435
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM)		2,943 33,842.95 16.221 July 16:00 12.435 3.785
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM) Peak Heating Load (W)		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM)		2,943 33,842.95 16.221 July 16:00 12,435 3.785 16.295 6,927.9
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Airflow (CFM) Peak Heating Load (W) Peak Heating Airflow (CFM) Checksums		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295 6,927.9 -14,253 626.6
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Latent Load (ton) Peak Heating Load (W) Peak Heating Airflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> )		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295 6,927.9 -14,253 626.6 208.65
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM) Peak Heating Load (W) Peak Heating Airflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> ) Cooling Flow Density (L/[s-m <sup>2</sup> ])		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295 6,927.9 -14,253 626.6 208.65 11.96
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Heating Load (W) Peak Heating Airflow (CFM) Peak Heating Airflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> ) Cooling Flow Density (L/[s-n <sup>2</sup> ]) Cooling Flow / Load (L/[s-kW])		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295 6,927.9 -14,253 626.6 208.65 11.96 57.32
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Leant Load (ton) Peak Cooling Leant Load (ton) Peak Heating Load (W) Peak Heating Airflow (CFM) Peak Heating Airflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> ) Cooling Flow Density (L/(s-m <sup>3</sup> )) Cooling Flow / Load (L/(s-kW)) Cooling Area / Load (m <sup>2</sup> /kW)		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295 6,927.9 -14,253 626.6 208.65 11.96 57.32 4.79
Inputs Building Type Area (ft <sup>2</sup> ) Volume (CF) Calculated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Leant Load (ton) Peak Cooling Leant Load (ton) Peak Heating Load (W) Peak Heating Airflow (CFM) Peak Heating Airflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> ) Cooling Flow Density (L/(s-kW))		2,943 33,842.95 16.221 July 16:00 12.435 3.785 16.295 6,927.9 -14,253 626.6 208.65 11.96 57.32

Fig 3.5 Without modification Result

To conclude with, we could find out the total tonnage require for centralised ac without any of Low Energy Cooling Technique & passive cooling techniques is 16.22ton

### 3.10 Method -2 With Modification:-

In order to verify the reduction in heat load require we consider the passive cooling techniques modification & low energy colloing technique

### **Reflective film :**

Reflective films is a passive cooling technique commonly used in architecture and automotive industries to reduce heat gain from sunlight. It involves applying a thin film or coating to windows or other surfaces that reflects a portion of the incoming solar radiation, thus reducing the amount of heat that enters a building or vehicle.

### **Roller blinds:**

Roller blinds are a simple and effective passive cooling solution that is widely used in buildings to reduce solar heat gain and improve thermal comfort Roller blinds can be mounted on windows to prevent or limit direct sunlight from entering a building's interior. The use of roller blinds serve to reduce solar heat gain by limiting the amount of sunlight that enters the space, keeping the indoor temperature lower. Roller blinds come in a variety of materials, including reflecting coatings and opaque textiles. These materials can reflect some of the sunlight away from the window or completely block it, lowering the amount of heat that enters the structure. Some roller blind materials offer additional insulation, which can help reduce heat transfer through windows in both hot and cold weather.

### **Gypsum wall partition:**

Gypsum partition walls can contribute to maintaining a comfortable indoor temperature by providing thermal mass, insulation, and aiding in the distribution of cool air throughout the building. Thickness of the gypsum is 6 inch

### **3D Floor Design**



Fig 3.16 With modification 3D Design

location and Weather	
Poject	Project Name
Address	
Calculation Time	12 April 2024 13:14
Report Type	Standard
Latitude	19.14°
Longitude	72.88°
Summer Dry Bulb	32°C
Summer Wet Bulb	25°C
Ninter Dry Bulb	D.C
Mean Daily Range	6°C
Building Summary	
Inputs	
Building Type	Office
Area (ft <sup>2</sup> )	2.943
	33,342.95
Calculated Results	33,842.95
Calculated Results Peak Cooling Total Load (ton)	33,842.95
Calculated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour	33,842.95 12,086 July 15:00
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Worth and Hour Peak Cooling Sensble Load (ton)	33,842.95 12,086 July 15:00 8.284
Iclume (CF) Calculated Results Reak Cooling Total Load (ton) Reak Cooling Sensible Load (ton) Reak Cooling Latent Load (ton) Reak Cooling Latent Load (ton)	33,842.95 12,086 July 15:00 8:284 3:802
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton)	33,842.95 12,086 July 15:00 8,284 3,802 11,655
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latert Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM)	33,842.95 12,086 July 15:00 8.284 3.802 11,655 4,309.5
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latert Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM) Peak Heating Load (M)	33,842.95 22,086 July 15:00 8:284 3:802 11:655 4:309.5 -14,204
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Arflow (CFIV) Peak Heating Linflow (CFIV) Peak Heating Linflow (CFIV)	33,842.95 12,086 July 15:00 8.284 3.802 11,655 4,309.5
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latert Load (ton) Peak Cooling Latert Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Arflow (CFM) Peak Heating Load (M) Peak Heating Airflow (CFM) Checksums	33,842.95 22,086 July 15:00 8:284 3:802 11:655 4:309.5 -14,204
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Arflow (CFIV) Peak Heating Arflow (CFIV) Peak Heating Arflow (CFIV) Checksums Cooling Load Density (Wi(m <sup>2</sup> )	33,842.95 12,886 July 15:00 8.284 3.802 11.655 4.309.5 -44,204 526.7
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Airflow (CFM) Peak Heating Load (M) Peak Heating Airflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> ) Cooling How Density (L/(s-m <sup>2</sup> ))	33,842.95 22,886 July 15:00 8.284 3.802 11.655 4.309.5 -14,204 526.7 155.47
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton) Peak Cooling Latent Load (ton) Maximum Cooling Capacity (ton) Peak Cooling Airflow (CFM) Peak Heating Load (M) Peak Heating Load (M) Peak Heating Liflow (CFM) Checksums Cooling Load Density (W/m <sup>2</sup> ) Cooling Flow Density (L/(s-m <sup>2</sup> )) Cooling Flow / Load (L/(s-m <sup>2</sup> )) Cooling Flow / Load (L/(s-m <sup>2</sup> ))	33,842.95 22,886 July 15:00 8.284 3.802 11.655 4.309.5 -44,204 626.7 155.47 7,44
Cakulated Results Peak Cooling Total Load (ton) Peak Cooling Month and Hour Peak Cooling Sensible Load (ton) Peak Cooling Latent Load (ton)	33,842.95 12,086 July 15:00 8.284 3.802 11.655 4.309.5 -44,204 626.7 155.47 7.44 47.85

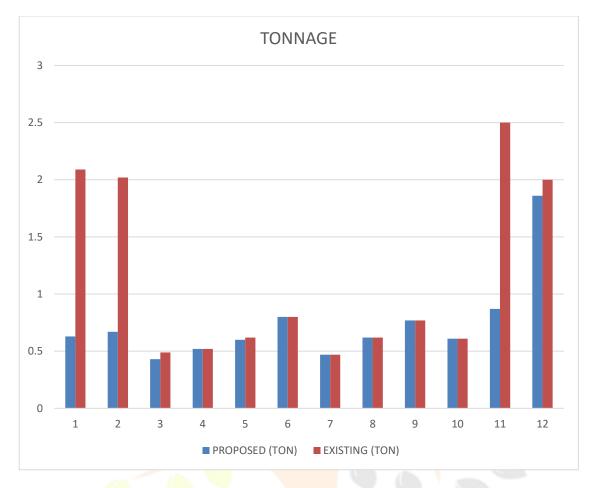


Considering Modification, we could find out the total tonnage required for VRF AC system by using Low Energy Cooling Technique & passive cooling techniques is 12.08 ton.

Percentage reduce in heat load due to modification

=[(16.22-12.08)/16.22]x100 Rezearch Through Innovation

=25.52%



### **Tonnage Comparison**

Fig 3.8 Tonnage Comparison with modification & without modification for rooms

different

### Heat Load Sheet (E20)

HVAC	LOAD	CALCU	JLATIC	N - E2	0 FOR	M SHE	ET			INPUT VALUES AR	E TO BE GIVE	N IN BLU	ECOLORI	BOXES ONLY	
PROJECT	Office								-	FLOOR 11th Room					
LOCATION				1.8	lumbai, Su	burban				SPACE REFERENCE	903/Commercial Floor(MUMEA)			6)	
CLIENT					XYZ	3				AREA ( Soft) (WsH) 3,300			30M		
CONSULTANT					ABC					Falce Ceiling Height (Pt)					
126.00	1						Volane (CuPt)						1	0.00	
	-	Area or		-	Sun Gain o	×	Farter			Estimate for				INNE	
item		Guantity			Temp. Diff		10	BtuHour	Watts	Design Conditions	70	B((F)	W8(f)	RH(%)	HR (Gritb)
					temp.usi			30.25.25	No.						
	_	ROOM HE	IRI		1	10	4年以前	۵ı	<u>.</u>	Ambient/Out Side		520	82.20	62.00	1000
ROOM SENSIBLE HEAT					_	-		8 <u></u>	6 - 2	Room (InDoor)		2.00	65.00	55.00	64,16
Solar Gain - Glass	Area			AT.			U			Difference &	2	3.20	17.20	5.08	56.00
Glass - N	1	SoPt	π			1	1.000	0.00		-			10 - D		
Gass-NE		SeR	I			1		0.00							
Glass - E	457.61	SaR	I	54.00	-	1	0.30	1,835,40		By Pass Factor (BF)					= 0.08
Gast-SE	-	SeR	1		_	I		0.00		Contact Factor (CF = 1 - BF)					= 0.94
Gaes - S		SaR	I		-	1		0.00	-		CFM Ve	distant.			
Glass - SW	-	Stift		-	_	1		0.00		CFW Per Person	5.00	No	- 1	72.00	= 380.00
to the second seco			I	-	-	_			-						
Gass-W	-	SAR	X	-	-	1		0.00	-	CRM Per SpPt	0.06	Set		3,300.00	= 198.00
Gaes - NW	-	SePt	X		-	1		0.00		Ar Charge Per Hour (CFM)	(222)		1996 E	-	1011224
Skylght.		SePt	x	1	-	- 1		0.00	-	CRI Cut	0.00	I	1.00	x160	= 0.00
Solar & Transmission Gain - Walls & Root			1								(CFN Int	000613			
Wall - N	9875		х	1200	F	I	0.29	3,301.65		Swinging		Т		chnidoor	= 00
Wal-NE		SaR	x		F	1		0.00	()	Revolving Doors (People)		1	10000	cfinidoor	= 0.0
Wall - E		392 332	x		F	1		0.00	1	Open Doors		1	捕	chridoer	= 0.0
Wal-SE		SeR	X		F	1		0.00		Crack (feet)	42.00	1	8.00	र्वफर्मि	= 252.0
Wal-S	948.75		I	15.30	F	T	040	6.944.85	-						252.0
Wal-SW	97613	the second second		10.00	F	_	144	0.00	-		Supply CFM f	Trans Manah	50		GL
		SUP	x	10.00		1			-		Stelleral	1001 #4600	ne -		-
Wal-W	437.00		I	E.I	F	1	040	3, 198, 84	-	Effective Room Sensible Heat Factor =	10.00				25 125
Wal-NW	1000	SIR	T.		F	1		0.00		Effective Room Sensible Heat/Eff Room Tota					= 03
Roof		SaPt	X		F	1		0.00			Apparatus Del	e?mxiA	2		
Transmission Gain - Except Walls & Roof		and the second			-	1	1000	1000000		indicated ADP (*F)					=
Al Gass	訂協	SaR	x	2326	F	1	0.30	188.62		Selected ADP (HF)					= 54.6
Partition	45	SiP	x	\$8.20	F	I	8.50	410.07	-		Dehunió	Sel Rice	_		
Ceirg	1300-00		I		F	1		0.00		Room DB - ADPI & CF		and there			= 18.3
Faor	3 300 00			18.20	F		0.27	18,218,20	-	DEHUMOIFIED AIR QUANTITY					144
NAMES OF TAXABLE PARTY OF TAXABLE PARTY.	0,000,00	ogn:	x	10.49	1	1	14.67	12,210,20	-	The second se					
INFLITRATION AND BY PASSED AR	L.CORES	and a		Sec. 1	1-11	1	income.	-const	2 3	Effective Room Sensible Heat			-	7,563.30	CFM
Infibration	252.00		x	22.20	T.D#	1	1.08	6,314.11	-	Dehumidified Rise x 1.08					
Outside Air	558.M	OFM	I	21.20		1	1	838.87							
Internal Heat	100000	1000	1000	1000	-			10110-01		1			-	3,554,75	Lis
People	72.00	Nos.	x	230.00	Btu Hour ?	Per Person		16,560,00		TOTAL HEAT CAPACITY					
hadwee	3,300,00	and the second sec	I	1.00	WISaPI	1	3.41	11,253,00		Grand Total Heat			-	16.07	TR
Lighting	Comparison in succession	_	. A							Care los res					in
Equipments	72.00			200.00	Wats	1	341	49,104.00		-					
Power	and a	間時	x					0.00		-					
Sub							-	1,16,175.51							
Fac	dor						5156	17,428.33							
Effective Room	Sensible	Heat						1,33,681,83	1.00	SENSIBLE HEAT CAPACITY					
ROOM LATENT HEAT	-									Grand Sensible Heat			(a)	16.07	TR
INTERIOR COLORIZATION	252.00	CEU .	I	5.0	(SIL)	1	0.68	9,596,16		12,000,00			200	real	305
Outside Ar	100		1	500		I	BFx0.68	1,274,92		100000					
							07,40,00		-	-					
People	72.00	1405.	X	120,00	Bts/Hour 8	rei reison		0.040.5	-						
Sub				_	-	-	52 M	10,511.08	-	+					
Fac					-		25-5%	975.55	-						
Effective Roor	n Latent H	iezt						21,486.63	2.00						
EFFECTIVE ROOM TOTAL HEAT			1	2		1		1,54,088,47	1000	1					
The Transmission		OUTSIDE	AIR HEAT							1					
Sensible	558.00	-	I	in the second	FITD	1	CEVI00	13,142,37	3.00	1					
				-	Sector Sector			the second s		+					
Latert	538.00	UHI	X	2.00	Grlb	1	CF-x0.68	18,673,72	4.00						
OUTSIDE AIR TOTAL HEAT		1		1		1		33,116.09		Notes					1
GRAND SUB-TOTAL HEAT								1,87,294.56							
Fac	tor						1-36	5,616,14		1					
GRAND TOTAL HEAT			1			10. J	To reaction in	1.92 620 70		1					
					1	1	T/BH	1000		1					
	-	-	-				TKW	552		1					
							TSMBH.	1.46.744.21	-	4					
								42,555,82	-	+					
							TSKI		_	4					
TONS=GRAND TOTAL HEAT/12000				1			1	1647							

Fig Heat load calculations for existing system

## Rezearch Through Innovation

### © 2024 IJNRD | Volume 9, Issue 5 May 2024| ISSN: 2456-4184 | IJNRD.ORG

HVAC	LOAD	CALCI	ILATIO	N - E20	FORM	SHEET	Č.			NPUT VALUES ARE TO	BE GIVEN IN	BLUEC	OLOR BOX	ES ONLY	
PROJECT					Office					FLOOR			118	for	
LOCATION					untai Subu	रेका ें				SPACE REFERENCE	_	903	Connercia	Foor MUNE	40
CLENT	-				192				_	AREA   SoF6 (Mp.H)				100	
CONSULTANT	<u> </u>				ABC					Falze Caling Height (P)					
1X.II				~						Volume CuPO			. 0	50	
		Area or	_		Sun Gain or		1	and the second		Estimate for			Sat	nter	
len		Quartity			Tenp Diff.		Factor (U)	Bulliour	Reb	Design Conditions	08	(19)	VB(15)	_	ROUN
	-	ROOM HE	37	-			0-1731		-	ArbientOut Side	妊		82.20	5.0	74.00
ROOM SENSIBLE HEAT		South State	a.		_		INC.		-	Room InDeerl	72		新師	55.00	64,00
	Ana	-	-	đ	-	_		-	-	Ofference 1	1	100.00	17.20	5.00	5.0
Solar Gain - Gass	<u></u>	SuP		-				0.00	-	Chiedrana 1			0.40	3.00	
Gass-NE	-	San San	I	-		I		0.00	-	-					
personal second s	-	-	I	-	-	x			-						1.00
Gen-E Gen-SF	47.00	Soft Soft	I	14.00	-	X	0.37	2.2年1月日 0月日	-	(By Plass Factor (BF) Contact Factor (CF = 1 - BF)					= <u>106</u> = 194
			I		-	I			-	(Grac race (2*+1+5*)	<b>CFN Vertial</b>	-			1 156
Gass-S		SoR	I	-	-	I	-	0.00	-		520	10		20.40	104.04
Gas-Sil	-	SaR	I		-	X		0.00	-	CRI PerPesan	The second second			72.00	= 360.00
Gass-W Gass-W	-	Soft Soft	1			T		0.00	-	(CRI/PerSyR Ar Darge PerHour (CRI)	0.05	Set	1	1,306.00	= 19E.00
and the second s		SoP1	I			X		0.00	-	(Ar Garge Her Hour (UNV) ICRV Cut	1.00		8.00	x160	- 0.00
Shipt	-	245	1	-		1			-	VIII VAII	CFN infibut	1	1.16	1:00	· 120
State & Construction Gast - Wells & Reed	948.75	2.0		42.00	F	-	4.00	1.747.45			C. MILLING		11		
Nel-N	56/3		X	12.00	F	X	0.37	4,212,45	-	Skitging Duration		I		chibor	= 0.00
Mal-NE		SeR	X		F	x		0.00	-	Revolving Doors (People)		x	1.32	chittor chittor	= 0.00 = 0.00
Wel-E		Soft Soc	X		F	X			-	Open Doos	100.00	x	100000000	( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	
Wel-SE	948.75	Soft	3		F	x		0.00 1346	-	Caok (test)	之田	x	6.90	dat	= 252.00
Nel-S	98/3		x	23	_	I	640		-			10 miles			252.90
Nel-50		SaR.	I		F	I		0.00	-		and ACC years	CHARGE .	5		
Mal-W	437.01		I	1830	F	x	0.40	3,193,84	-	Effective Room Sensible Heat Factor =					
Wel-NW		SaR	x	-	F	I		0.00	-	Effective Room Sensible Heat Eff Room Total Heat		Contraction of the local division of the loc			= 0.83
Red	-	SqR	x	-	F	I	-	0.00	-		peratus Dew Pro	10.000	si.		
Terrinen Ger-Ever Heb 3 Ref	-								-	Indicated ACP (17)					-
Al Gas	_	Seff	1		F	I	0.30	0.00	-	Selected ADP (F)					= 54.51
Patien		SaR	I	58	F	X	8.58	0.00	-		Debut offer				
Ceiling	3382		x	19話	F	X	0.27	15,215.20	-	Roon DB - ADP) = DF					= 16.35
Foor	1300.00	Str.	I	1820	F	X	0.27	16,216.20	-	DEHLMIDIFIED AIR QUANTITY					
NELTRICK HOBY PRSSED AR									-	Effective Room Sensible Heat			=	1949	ORM
ोगीडांका	22.95		x	_	101	X	158	6314.11	-	Detunidiled Rise x 1.08					
Outside Air	玩評	Q-M	1	22		I		538.87	-	-					
Riema Telle				-					-					2,991,67	Us
People	-	No.	X	_	Bullour P		-	16,582.00	-	TOTAL HEAT CAPACITY				1000000	
Lighting	3,301.00	St/R	x		NSqP:	X	3.41	11,252.00		Grand Total Heat			- 1	12.95	12
Equprents	1.00			200.00	Rats	1	341	682.00		1					
Poer		101	T					0.00		1					
	100				-		-	展700.19	-	1					
Fa	tų –						5-155	12,705.03							
Effective Room	Sersible	Heat						97,48521	1.00	SENSIBLE HEAT CAPACITY					
ROOM LATENT HEAT		1								Grand Sensible Heat				12.96	R
Initation	252,01	031	.1	我族	665	х	088	9,595,18		12,000.00					
Outside Air	59.8		I	5.0	GLb	I	3Fx168	1,274,92	1	1					
People	72.00	NC5.		調整	Bullour?	erPetan		854135		1					
Sab	īdal			-				19,511,08		1					
Fa	for .						25-5%	975.55		1					
Effective Roo	e Latert H	eat						22,486.63	2.00						
EFFECTIVE ROOM TOTAL HEAT			-					切割酒		1					
		OUTSIDE	紙紙紙							]					
Sensble	現居	(CRII	x	23.20	府国	х	(Fat.08	13,142.37	3.00	1					
Løert	59.11		I	5.3		x		19,973,72		1					
OUTSIDE AR TOTAL HEAT	-		-				a sud	13,115,09		Neter		_			
	-			-		-	-	19,110,04	-	Netes					
GRAND SUB-TOTAL HEAT	for .					-	1.15	4,531,24	-	1					
GRAND TOTAL HEAT					-		1.1.20	12225		1					
		-	1		-		THEN	1553		1					
							101	4511		1					
							_	111575		1					
							TSKIN	12/58.80		1					
TONS=GRAND TOTAL HEATINGON								12.56		1					
								Million and Add	-	1					

Fig Heat load calculations for Proposed system

#### IV. RESULTS AND DISCUSSION

Sr. No.	Name	Number of Quantity	Single quantity cost	Total quantity cost	Installation cost	Total cost
	1 Outdoor unit [35 HP]	2	100000	200000	20000	220000
	2 Casssette 1.5TR	11	48000	528000	52800	580800
	3 Casssette 2.0TR	2	65000	130000	13000	143000
	4 Copper pipe	30m	650 per meter	20000	2000	22000
	5 Gypsum Standard Board	3000 sq ft	. 85 per sq ft	255000	25000	280000
	6 Dehumidifier [40 pints]	2	22000	44000	4000	48000
	7 Passive Technique	440 sq ft	75 per sq ft	54136	5400	59536
				1210000	122200	1332200

Fig Proposed System								
	A	В	С	D				
1	ANNUAL OPERATING COST	EXISTING	PROPOSED					
2	COST OF ENERGY	681366	724530					
3	COST OF WATER	275520	0					
4	MAINTANENCE COST	80240	95230					
5	TOTAL COST	1037126	819760					
6								
7								

### Fig Annual Running Cost

### **Conclusion:-**

A sustainable HVAC system's major purpose is to provide thermal comfort while using the least amount of energy possible, as well as suitable interior air conditioning and high-quality ventilation. Using theoretical and analytical methods, the energy consumed is 9100kw, and the running cost / life analysis cost is 7.2 LPA. The Proposed system will take a total of six years to return its costs. By using analytical methods The energy Consumed is reduced by 25.52% and the running life cost is lowered by 20.95%. The modified system will take a total of six years to return its cost.

### **References:-**

1. D.K. Bhamare, M.K. Rathod, J. Banerjee, Passive cooling techniques for building and their applicability in different climatic zones—the state of art, Energy Build. 198 (2019) 467–490, https://doi.org/10.1016/j.enbuild.2019.06.023. [1]

2. A.K. Nanda, C.K. Panigrahi, A state-of-the-art review of solar passive building system for heating or cooling purpose, Front. Energy 10 (2016) 347–354, https:// doi.org/10.1007/s11708-016-0403-0[2]

3. H. Goudarzi, A. Mostafaeisour, Natural and night-time ventilation Office buildings in hot and Humid Climate , Renew. Sustain. Energy Rev. 68 (2017) 432–446, https://doi.org/10.1016/j.rser.2016.10.002.[3]

4. Kartik Patel, Prof. Pushpendra K. Jain, Prof. Dinesh K. Koli Published a paper on Variable refrigerant flow (VRF). (VRF) is an air-condition system configuration where there is one outdoor condensing unit and multiple indoor units.[4]

5. Mohamed Elnaggar, Mohammed Alnahhal Publish a paper on central air conditioning systems based on the type of working fluid used for heating and cooling purposes[5]

6. A. T. Layeni1, C. N. Nwaokocha1, S.O.Giwa1, M.A Sulaiman1, K.A. Adedeji and A.I. Olanrewaju Publish a paper on the performance and economic feasibility of these VRF AC systems[6]

7. Blanco, E. Schettini, G. Scarascia Mugnozza , C.A. Campiotti, G. Giagnacovo, G. Vox published a research paper that addresses the various factors that influence indoor air temperature, including external air temperature, relative humidity, solar radiation, <u>wind speed</u>, building <u>materials</u>, and design variables.[7]

8. <u>Lin Pan</u>, <u>Sheng Wang</u>, <u>Jiying Wang</u>, <u>Min Xiao</u> and <u>Zhirong Tan</u> published a paper that examines the <u>energy consumption</u> and <u>efficiency</u> of central air conditioning systems in urban buildings.[8]

9. Mohammad Arif Kamal-, Sahil Ali Khan , <u>Variable Refrigerant Flow</u> (VRF) system, also known as Variable Refrigerant Volume (<u>VRV</u>), in comparison to traditional air-conditioning systems.[9]

10. Mat Santamouris, Passive cooling technologies for buildings in response to the increasing energy and environmental impact of <u>air conditioning</u> systems.[10]

11. Cooling Load calculations and principles by A. Bhatia, 2018 [11]

12. Annapureddy Sambasiva Rao, Mr.A Soma Raju, Ayub Ashwak, Harish Raj, USDR 2019. This paper includes a thorough design of an air distribution ducting system utilising the McQuay Duct Sizer[12]

13. Air Handling Unit by Venus Lun, 2020 [13]

14. ASHRAE Handbook 2005[14]

15. I Dewa Gede Arya Putra, Hideyo Nimiya, Ardhasena Sopaheluwakan, Tetsu Kubota publish a paper on , Development of climate zones for passive cooling techniques in the hot and humid climate of Indonesia[15]

16. Wan Iman Wan Mohd Nazi , Mohammad Royapoor, Yaodong Wang, Anthony Paul Roskilly,"
Office building cooling load reduction using thermal analysis method – A case study"by science direct
2015[16]

17. A. T. Layeni1, C. N. Nwaokocha1, S.O.Giwa1, M.A Sulaiman1, K.A. Adedeji and A.I. Olanrewaju Design and Engineering Economic Analysis of a Variable Refrigerant Flow (VRF) and Mini-Split Air Conditioning System[17]

18. Wan Iman Wan Mohd Nazi , Mohammad Royapoor, Yaodong Wang, Anthony Paul Roskilly," Office building cooling load reduction using thermal analysis method – A case study"by science direct 2015[18]

19. Xinqiao Yu, Da Yan, Kaiyu Sun, Tianzhen Hong, Dandan Zhu,"Comparative study of the cooling energy performance of variable refrigerant flow systems and variable air volume systems in office building[19]

20. Oleksandr tanskyi, Analysis of Innovative HVAC System Technologies and Their Application for Office Buildings in Hot and Humid Climates, December 2010[20]

21. Mohammad Arif Kamal publish a paper on An overview of passive cooling techniques in buildings: Design concepts and architectural interventions[21]

22. Oleksandr tanskyi, Analysis of Innovative HVAC System Technologies and Their Application for Office Buildings in Hot and Humid Climates, December 2010[22]

23. Lain, M., Drkal, F., Hensen, J.L.M. & Zmrhal, V. (2004). Publish a paper on Low energy cooling techniques for retrofitted office buildings in central Europe[23]

24. ISHRAE Handbook 2007[24]

